525 Rec'd PCT/PTO 27 NOV 2000 ØRM PTO-1390 (Modified) U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE TRANSMITTAL LETTER TO THE UNITED STATES 587-68 EPO/PCT/US\_ DESIGNATED/ELECTED OFFICE (DO/EO/US) U.S. APPLICATION NO. (IF KNOWN, SEE 37 CFR 701223 CONCERNING A FILING UNDER 35 U.S.C. 371 INTERNATIONAL APPLICATION NO. INTERNATIONAL FILING DATE PCT/US99/11617 26 May 1999 (26.05.99) 27 May 1998 (27.05.98) TITLE OF INVENTION APPARATUS AND METHOD FOR TESTING A TELECOMMUNICATIONS SYSTEM APPLICANT(S) FOR DO/EO/US Robert De Tullio; Mark Greening; Jiliang Yu and John Kelvin Fidler Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following stems and other information: This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 3 This is an express request to begin national examination procedures (35 U.S.C. 371(f)) at any time rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b) and PCT Articles 22 and 39(1). A proper Demand for International Preliminary Examination was made by the 19th month from the earliest claimed priority date. A copy of the International Application as filed (35 U.S.C. 371 (c) (2)) a. 
 is transmitted herewith (required only if not transmitted by the International Bureau).
 h П has been transmitted by the International Bureau. is not required, as the application was filed in the United States Receiving Office (RO/US). A translation of the International Application into English (35 U.S.C. 371(c)(2)). A copy of the International Search Report (PCT/ISA/210). Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371 (c)(3)) a. 🗆 are transmitted herewith (required only if not transmitted by the International Bureau). b. 🗵 have been transmitted by the International Bureau. c. 

have not been made; however, the time limit for making such amendments has NOT expired. d  $\square$ have not been made and will not be made. 9.3 A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)). 16.3 An oath or declaration of the inventor(s) (35 U.S.C. 371 (c)(4)). A copy of the International Preliminary Examination Report (PCT/IPEA/409). 12. A translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371 (c)(5)). Items 13 to 20 below concern document(s) or information included: An Information Disclosure Statement under 37 CFR 1.97 and 1.98 An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included. A FIRST preliminary amendment A SECOND or SUBSEQUENT preliminary amendment A substitute specification. A change of power of attorney and/or address letter.  $\boxtimes$ Certificate of Mailing by Express Mail Other items or information: (1) Copy of the international application as published on 2 December 1999 under publication number WO 99/62188.

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  - (2) Copy of Article 34 Amendment.

SZY NEC O PULIPIT 27 NOV 2000 U.S. APPLICATION NO / 1701 223 INTERNATIONAL APPLICATION NO ATTORNEY'S DOCKET NUMBER PCT/US99/11617 587-68 EPO/PCT/US 21 The following fees are submitted: CALCULATIONS PTO USE ONLY BASIC NATIONAL FEE ( 37 CFR 1.492 (a) (1) - (5)) : Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2) paid to USPTO and International Search Report not prepared by the EPO or JPO \$1,000.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but Internation Search Report prepared by the EPO or JPO \$860.00 \$710.00 International preliminary examination fee paid to USPTO (37 CFR 1.482) but all claims did not satisfy provisions of PCT Article 33(1)-(4) . . . . \$690.00 International preliminary examination fee paid to USPTO (37 CFR 1.482) and all claims satisfied provisions of PCT Article 33(1)-(4)...... \$100.00 ENTER APPROPRIATE BASIC FEE AMOUNT = \$690.00 Surcharge of \$130.00 for furnishing the oath or declaration later than months from the earliest claimed priority date (37 CFR 1.492 (e)). \$0.00 CLAIMS NUMBER FILED NUMBER EXTRA RATE Total claims - 20 = n v \$18.00 \$0.00 Independent claims - 3 = I \$80.00 \$80.00 Multiple Dependent Claims (check if applicable) \$0.00 TOTAL OF ABOVE CALCULATIONS \$770.00 Reduction of 1/2 for filing by small entity, if applicable. Verified Small Entity Statement must also be filed (Note 37 CFR 1.9, 1.27, 1.28) (check if applicable). \$0.00 SUBTOTAL \$770.00 Processing fee of \$130.00 for furnishing the English translation later than 20 □ 30 months from the earliest claimed priority date (37 CFR 1.492 (f)). \$0.00 TOTAL NATIONAL FEE \$770.00 ec. for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31) (check if applicable). \$0.00 TOTAL FEES ENCLOSED = \$770,00 Amount to be: refunded \$ \$ charged X A check in the amount of \$770.00 to cover the above fees is enclosed. Please charge my Deposit Account No. in the amount of to cover the above fees. A duplicate copy of this sheet is enclosed. The Commissioner is hereby authorized to charge any fees which may be required, or credit any overpayment to Deposit Account No. 08-2461 A duplicate copy of this sheet is enclosed. NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137(a) or (b)) must be filed and granted to restore the application to pending statu SEND ALL CORRESPONDENCE TO: Gerald T. Bodner, Esq. Hoffmann & Baron, LLP SIGNATURE 6900 Jericho Turnpike Syosset, New York 11791 Gerald T. Bodner United States of America NAME 30,449 Phone (516) 822-3550 Facsimile (516) 822-3582 REGISTRATION NUMBER

November 27, 2000 DATE 587-68 EPO/PCT/US

529 Rec'd PCT/PTC 27 NOV 2000

## IN THE U.S. DESIGNATED/ELECTED OFFICE OF THE PCT

IN RE APPLICATION OF: Robert De Tullio, et al.

INTERNATIONAL APPLICATION NUMBER: PCT/US99/11617

INTERNATIONAL FILING DATE: 26 May 1999

FOR: APPARATUS AND METHOD FOR TESTING A TELECOMMUNICATIONS: SYSTEM

Assistant Commissioner for Patents BOX PCT Washington, DC 20231 ATTENTION: DO/EO/US

#### EXPRESS MAIL CERTIFICATE OF MAILING FOR ABOVE-IDENTIFIED APPLICATION

Express Mail" mailing label number: EL633571378US

Date of Deposit: November 27, 2000

I hereby certify that the enclosed <u>Transmittal Letter</u> to the United States Designated/Elected Office Concerning a Filing Under 35 U.S.C. 371 (in duplicate); copy of International Publication <u>Number WO 99/62188</u>; International Search Report; copy of Article 34 Amendment; check for \$770.00; and return receipt postcard is deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 C.F.R. §1.10 on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, DC 20231.

Lisa Bartell

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Printed Name of person mailing paper

Signature of person mailing paper

### IN THE INTERNATIONAL PRELIMINARY EXAMINATION AUTHORITY

Applicant:

Porta Systems Corporation, et al.

Authorized Officer:

Curtis Kuntz/Rugenia Logan

International Application No.:

PCT/US99/11617

Group Art Unit:

Unassigned

Int'l Filing date:

May 26, 1999

Docket:

587-68 EPO/PCT

Dated:

September 15, 2000

APPARATUS AND METHOD FOR TESTING A

TELECOMMUNICATIONS SYSTEM

For:

Commissioner of Patents and Trademarks

Box PCT

Washington, D.C. 20231

#### RESPONSE TO WRITTEN OPINION

Applicants request amendment of the above-identified International Application under

Article 34 as set forth below:

#### In the Claims:

Please substitute Application pages 20-22 with replacement sheets 20-22.

#### REMARKS

This Amendment to the International Application under Article 34 replaces originally filed Claims 3-7 with amended claims bearing the same numbers. These amendments have previously been submitted in an Amendment under Article 19, which was filed in the

September 15, 2000

Sir:

14 1 International Bureau on February 15, 2000. However, in view of the Examiner's comments in the Written Opinion concerning Claim 4, Applicants hereby resubmit the amendments contained herein.

Applicants respectfully request entry and consideration of this Amendment under Article 34 in preparing the International Preliminary Examination Report.

Respectfully submitted,

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#### CLAIMS

- A method of testing a telecommunications system, the method comprising;
- applying a first AC test signal having a first signal frequency to the system and measuring the response of the system to the first test signal;
- 2) applying a second AC test signal having a second signal frequency different to the first signal frequency to the system and measuring the response of the system to the second test signal; and
- 3) calculating one or more parameters of the system after the responses measured in steps 1) and 2).
- $^{\frac{1}{2}}$  2. A method according to claim 1 wherein the first and  $^{\frac{1}{2}}$  second test signals are applied at different times.
- 3. A method according to claim 1 wherein one or both of the litest signals has a substantially sinusoidal waveform.
- $^{\circ}_{1}$  4. A method according to claim 1 wherein less than five cycles  $\mathbb{P}$  of each signal is applied to the system.
- $\frac{\pi}{\sqrt{5}}$ 5. A method according to claim 1 wherein the test signals  $\frac{\pi}{\sqrt{5}}$  are each applied to the system through a known impedance.
  - A method according to claim 1 further comprising applying;
  - applying one or more additional test signals to the system and measuring the response of the system to at least one test signal; and
  - wherein step 3) comprises calculating one or more parameters of the system from the responses measured in steps 1),2) and 4).
  - 7. A method according to claim 1 wherein the system comprises first and second transmission lines, and wherein each step of applying a test signal and measuring the response of the system comprises

- a) applying the test signal to the first line and monitoring the response of the first line and the second line to the test signal; and
- b) applying the test signal to the second line and monitoring the response of the second line and the first line to the second test signal.
- 8. A method of testing a telecommunications system comprising first and second transmission lines, the method comprising
- applying a first test signal to the first line and measuring the response of the first line and the second line to the first test signal;
- 2) applying a second test signal to the second line and we measuring the response of the second line and the first line to the second test signal; and
  - 3) calculating one or more parameters of the telecommunications system from the responses measured in steps 1) and 2).
- 9. A method according to claim 8 wherein the first and second signals each comprise AC signals.
- 10. A method according to claim 9 wherein the signal frequencies of the first and second test signals are substantially identical.
  - A method according to claim 10 wherein the first and second test signals have a known phase relationship.
  - Apparatus for testing a telecommunications system, the apparatus comprising;
  - means for applying a first AC test signal having a first signal frequency to the system;
  - means for measuring the response of the system to the first test signal;
  - 3) means for applying a second AC test signal having a second signal frequency different to the first signal frequency to the system;
  - means for measuring the response of the system to the second test signal; and

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- 5) means for calculating one or more parameters of the system from the responses measured in steps 1) and 2).
- 13. Apparatus for testing a telecommunications system comprising first and second transmission lines, the apparatus comprising
- means for applying a first test signal to the first line
- means for measuring the response of the first line and the second line to the first test signal;
- 3) means for applying a second test signal to the second line;
- 4) means for measuring the response of the second line and the first line to the second test signal; and
- \$\frac{13}{2}\$ 5) means for calculating one or more parameters of the \$\frac{12}{2}\$ telecommunications system from the responses measured in steps \$\frac{13}{2}\$ 1) and 2).

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## APPARATUS AND METHOD FOR TESTING A TELECOMMUNICATIONS SYSTEM

The present invention relates to a method and apparatus for testing a telecommunications system.

Conventional apparatus for testing telecommunications systems applies a test signal to the telecommunications system and, by analysing the response of the system to the test signal, calculates one or more parameters of the system in accordance with a chosen line model.

A problem with conventional methods is that it is not possible to determine the series line resistance of a transmission line in the system under test.

In accordance with a first aspect of the present invention there is provided a method of testing a telecommunications system, the method comprising;

- applying a first AC test signal having a first signal frequency to the system and measuring the response of the system to the first test signal;
- applying a second AC test signal having a second signal frequency different to the first signal frequency to the system and measuring the response of the system to the second test signal; and
- calculating one or more parameters of the system from the responses measured in steps 1) and 2).

The first aspect of the present invention provides additional data which can be analyzed to calculate system parameters (e.g. electrical parameters such as resistance or capacitance) which have been previously difficult or impossible to determine - such as series line resistance.

The first and second AC test signals may be applied at the same time, in the form of a multi-frequency signal. However preferably the first and second test signals are applied at different times.

35 The wave form of the first and/or second test signal may be non-sinusoidal (for instance a square wave or sawtooth wave) but preferably the test signals have a

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WO 99/62188 PCT/US99/11617

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substantially sinusoidal waveform. This simplifies the calculation procedure.

It is important that the method can test the telecommunications system quickly - this enables a number of lines within the system to be tested over a given period. Therefore preferably less than 5 cycles of each signal is applied to the system. In a preferred embodiment, two cycles of each signal are applied to the system.

Typically the test signals are each applied to the system through a known impedance. The voltage drop across the known impedance can then be used to calculate a characteristic impedance of the telecommunications system.

If additional data is required, then one or more additional test signals may be applied to the system. The one or more additional test signals may comprise AC test signals with a signal frequency different to the signal frequency of the first and second test signals. However preferably the or each additional test signal comprises a DC test signal.

Typically the system comprises first and second transmission lines (conventionally known as A and B lines). Conventionally an AC test signal is applied simultaneously to both lines (either in phase or in anti-phase) and the response of only one of the lines is monitored. In a preferred embodiment the step of applying a test signal and measuring the response of the system comprises:

- a) applying the test signal to the first line and monitoring the response of the first line and the second line to the test signal; and
- b) applying the test signal to the second line and monitoring the response of the second line and the first line to the second test signal.

By monitoring the response of both lines, additional parameters can be obtained.

In accordance with a second aspect of the present invention there is provided a method of testing a

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telecommunications system comprising first and second transmission lines, the method comprising

- applying a first test signal to the first line and monitoring the response of the first line and the second line to the first test signal;
- 2) applying a second test signal to the second line and monitoring the response of the second line and the first line to the second test signal; and
- calculating one or more parameters of the telecommunications system from the responses measured in steps 1) and 2).

The second aspect of the present invention enables a number of system parameters to be calculated. In contrast with conventional systems, the response of both the first line and the second line is monitored.

The first and second signals may be DC signals, or alternatively the first test signal and/or the second test signal may comprise an AC signal. In a preferred example the signal frequencies of the first and second test signals are substantially identical. Alternatively, the signal frequency of the first and second test signals may be different.

The first and second test signals may be generated independently, but preferably they have a known phase relationship. This enables the parameters to be calculated more easily in step 3).

A number of embodiments of the present invention will now be described with reference to the accompanying drawings in which:-

Figure 1 is a schematic illustration of apparatus for testing a telecommunications system;

Figure 2 illustrates the remote test unit, exchange and telephone in more detail;

Figure 3 illustrates the functional structure of the remote test unit;

Figure 4 is a schematic diagram illustrating the arrangement of the line test unit;

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Figure 5 illustrates part of the measurement cycle; Figure 6 illustrates the full complex voltages measured by the AC measurement cycle;

Figure 7 is a first example of a line model;

Figure 8 is an enhanced line model;

Figure 9 is a line termination model, discussed in Appendix 4; and  $% \left( 1\right) =\left( 1\right) +\left( 1\right)$ 

Figure 10 is a third example of a line model.

Figure 1 is a schematic diagram of a system for remotely testing a telecommunications line. An operator station 1 is connected to a general controller 2 which inputs and outputs signals to/from a telecommunications medium 3 (which may comprise a PSTN or X.25 network). A telephone 6 is connected to a local exchange 5 via a land line 7. A remote test unit (RTU) 4 is connected to the exchange 5 in order to test the land line 7. Figure 1 illustrates a control path 8 and a test path 9.

As can be seen in Figure 2, the line 7 comprises a pair of lines 10,11 (configured as a twisted pair) known conventionally as "A" and "B" lines. An exchange feed comprising a 50V battery 12 is connected to the A and B lines 10,11 during normal operation via 200 ohm resistors 13,14. In order to test the line 7, the RTU control line 8 switches the A and B lines 10,11 over to the test line 9 (which in turn comprises a pair of input lines 15,16). The RTU communicates with the general controller 2 via a V.24 link (17) or 300 V.21 link (18).

The internal functional structure of the RTU 4 is shown in Figure 3. The A and B input lines 15,16 are connected to a line access unit 19 which controls the input and output of signals to/from the line 7. A line test unit 22 controls testing of the line 7, a tone generator 23 generates tone signals 24 which can be output onto the line 7, and voice modems 25,26 handle voice signals which can be communicated between the operator station 1 and telephone set 6. The RTU is controlled by a microprocessor 20 and data acquired is saved in a memory 21.

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The line test unit 22 is illustrated in more detail in Figure 4. A pair of signal generators 30,31 generate sine wave signals which are amplified by respective amplifiers 32,33. The signals output by amplifiers 32,33 have a range of +/-200V and a bandwidth of 10kHz. The signal generators 30,31 are run synchronously from the same clock by a controller 34. This ensures that the signals have a known phase relationship. Each line has a respective set of output resistors 35-40 (each having a known resistance within a tolerance of 1%). Each output resistor has an associated switch 41-46 which can be closed by controller 34 to connect the associated output resistor between the amplifier and output line 47,48. Typical resistance values for the three output resistors on each line are 200.1M and 100K ohms. The voltage on line A is measured by a voltmeter 49 and the voltage on line B is measured by a voltmeter 50. The voltages are digitised by A-D converter 51 which samples at 12 kHz. Phase and RMS voltage values are calculated by processor 52 and stored in memory 53.

Referring to Figure 5, the line test procedure is as follows:

Step 1 - open all output resistor switches 41-46 and measure DC voltage on A and B lines.

Step 2 - adjust DC bias of amplifier 32 so that amplified signal is centred on line A DC voltage level.

Step 3 - adjust DC bias of amplifier 33 so that amplified signal is centred on line B DC voltage level.

Step 4 - set signal generators 30,31 to generate a DC signal.

30 Step 5 - close a selected one of the line A output resistor switches 41-43.

Step 6 - store DC voltages on voltmeters 39,50 in memory 53.

Step 7 - open selected line A switch and close a selected one of the line B output resistor switches 44-46.

Step 8 - store DC voltages on voltmeters 39,50 in memory 53.

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Step 9 - set signal generators 30,31 to 2.75Hz.

Step 10 - after first cycle, perform digital fourier transform (at  $2.75 \mathrm{Hz}$ ) of signals from voltmeters 49,50 over second cycle and store amplitude and phase values in memory 53.

Step 11 - open selected switch 44-46 (line B) and close switch 41-43 associated with selected output resistor (line A).

Step 12 - after first cycle, perform digital fourier transform (at 2.75Hz) of signals from voltmeters 49,50 over second cycle and store amplitude and phase values in memory 53.

Step 13 - adjust frequency of signal generators 30,31 to  $5\mathrm{Hz}$ .

Steps 14-16 - repeat steps 10-12 at 5Hz.

The resulting AC data can be represented as four complex voltage values as illustrated in Figure 6, where:

 $\rm V_{A1}$  is the voltage measured by voltmeter 49 (line A) with signal being applied to line A;

 $V_{81}$  is the voltage measured by voltmeter 50 (line B) with signal being applied to line A;

 $\rm V_{A2}$  is the voltage measured by voltmeter 49 (line A) with signal being applied to line B; and

 $\rm V_{82}$  is the voltage measured by voltmeter 50 (line B) with signal being applied to line B.

The four complex values can then be used to calculate four impedance parameters Z as defined below:

 $Z_{11}=V_{ae}/I_a$  when line b is open;

 $Z_{22}=V_{he}/I_{h}$  when line a is open;

 $Z_{12}=V_{ae}/I_{h}$  when line a is open; and

 $Z_{21}=V_{he}/I_a$  when line b is open;.

where

 $V_{ae}$  is the voltage on voltmeter 49 (ie. the voltage from line A to earth);

35  $V_{be}$  is the voltage on voltmeter 50 (ie. the voltage from line B to earth);

I, is the current on line 47 (line A); and

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 ${\rm I_b}$  is the current on line 48 (line B).

Since the voltages  $(V_a,V_b)$  output by the amplifiers 32,33 and the values  $(R_a,R_b)$  of the resistors 35-40 are known accurately, the currents  $I_a$  and  $I_b$  can be eliminated from the expressions for Z as follows:

$$\begin{split} & Z_{11} = R_{a}V_{ae}/\left(V - V_{ae}\right); \\ & Z_{22} = R_{b}V_{be}/\left(V - V_{be}\right); \\ & Z_{12} = R_{b}V_{ae}/\left(V - V_{be}\right); \text{ and } \\ & Z_{21} = R_{a}V_{be}/\left(V - V_{ae}\right). \end{split}$$

Once the Z parameters have been calculated as discussed above, they can be used to determine characteristics of the line 7 under test using an algorithm based on a selected line model.

One example of a suitable line model is illustrated in Figure 7. The series resistances of the lines 10,11 between the RTU 4 and the telephone 6 are represented by resistors  $R_1, R_2$ . The line termination at telephone 6 is represented by resistors  $R_5, R_6$  and capacitors  $C_2, C_3$ . The leakage to ground from the A and B lines is represented by resistors  $R_5, R_6$  and capacitors  $C_1, C_2$ . The problem with the line model of Figure 7 is that it is difficult to find ten independent equations based on conventional tests in order to calculate the ten line model parameters. Even if ten independent equations could be found, it would be difficult to solve the ten non-linear equations even by a numerical method.

The alternative line model of Figure 8 reduces the number of parameters to be identified by replacing the line termination parameters  $R_5,R_6,C_2$  and  $C_3$  with a single impedance value Z. In Figure 8 the series resistances of the lines 10,11 between the RTU 4 and the telephone 6 are represented by resistors  $\mathbf{r}_1,\mathbf{r}_2$  and the leakage to ground from the A and B lines is represented by resistors  $\mathbf{g}_1,\mathbf{g}_2$  and capacitors  $C_1,C_2$ .

A set of equations based on the enhanced line model of Figure 8 can be manipulated into a linear equation system

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and a set of symbolic solutions obtained as set out in Appendix 1, Appendix 2 and Appendix 3 below.

Furthermore, the line termination parameters can also be calculated as set out in Appendix 4 below.

The calculated values of the parameters  $r_1$ ,  $r_2$ ,  $g_1$ ,  $g_2$ ,  $c_1$ ,  $c_2$  and z are stored at the RTU for later analysis or transmitted back to the operator station 1. The parameters can then be used to identify and characterise any faults on the line 7 such as a break in the line, fault to ground or fault to another line. Furthermore the parameters can be used to determine whether the line 7 is suitable for carrying different communication protocols such as ISDN\_DACS\_HDSL\_CWSS or ADSL.

A further alternative line model is illustrated in Figure 10. It is possible to calculate the parameters of this model using a simplified measurement procedure which uses a DC measurement followed by a single AC measurement (ie. at only one frequency).

Although the line test unit 22 illustrated in Figure 4 is shown with two signal generators 30,31 and two sets of output resistors 41-46, it will be appreciated that a single generator and a single set of resistors could be used, and switched from one line to the other.

#### Appendix 1

## Identification Results

The model parameters including the series resistances are given as follows,

$$\tau_{1} = \frac{r_{1}Z_{1_{10}} + Z_{1_{10}}\omega r_{2} + \omega r_{2}Z_{1_{20}} + Z_{1_{20}}}{\omega r_{2}}$$
(1)

$$r_{i} = \frac{n_{i}Z_{1/is} + Z_{11/is}\omega n_{i} + \omega n_{i}Z_{11/is} + Z_{11/is}}{\omega n_{i}}$$
(2)

$$g_z = -\frac{\omega r_z}{(r_z)^2 Z_{1,\mathbf{b}} + r_1 r_2 Z_{1,2,\mathbf{b}} \omega + r_1 Z_{1,2,\mathbf{b}} \omega + r_1 Z_{1,2,\mathbf{b}} \omega + r_2 Z_{2,2,\mathbf{b}} (\omega)^2 + (r_z)^2 Z_{1,\mathbf{b}} (\omega)^3}$$
(3)

$$g_1 = n_1 g_2$$

$$c_1 = \pi_1 g_2 \tag{4}$$

$$c_1 = n_1 g_1$$

$$Z = \frac{\frac{1}{Z_{1z}} - g_1 - g_2 - j\omega c_1 - j\omega c_2}{(g_1 + j\omega c_1)(g_2 - j\omega c_2)}$$
(6)

where  $\omega$  is test frequency,  $Z_{ja}$  and  $Z_{jib}$ , i=1,2, j=1,2 are the real and imaginary parts of the Z-parameters respectively, and  $n_{ib}$ , k=1,2,3 can be calculated from the knowns, whose expressions along with the detailed mathematical manipulations were given in the appendix.

## An example

For a simple example to show that the proposed method can solve the problem, let us suppose that

 $r_1 = r_2 = 1$ .

 $g_1 = 2$ ,

 $g_{2} = 3$ 

 $c_1 = 2$ 

 $c_{1} = 4$ 

 $Z = \frac{1 - j\omega}{\omega}$ 

For this simple example, the measurements of Z-parameters can be easily simulated by simple calculation as indicated in (7)-(9) in the appendix. They are,

$$\omega = 1,$$

$$Z_{tia} = \frac{377}{328}$$

$$Z_{11b} = \frac{328}{-51}$$

$$Z_{12u}=\frac{2}{41}$$

$$Z_{12b} = \frac{-5}{82}$$

$$Z_{22a} = \frac{45}{41}$$
$$Z_{22b} = \frac{-5}{41}$$

$$Z_{11a}^2 = \frac{10145}{9442}$$

$$Z_{11b}^2 = \frac{-711}{4721}$$

$$Z_{12a}^2 = \frac{50}{4721}$$

$$Z_{12b}^2 = \frac{-128}{4721}$$

$$Z_{22u}^2 = \frac{4896}{472!}$$

$$Z_{225}^1 = \frac{-488}{4721}$$

substitue them to (27) to (35) to calculate coefficients (See appendix 2 for definition) we get

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$$a_1 = \frac{116037}{1548488}$$

$$a_2 = \frac{7392}{193561}$$

$$a_1 = \frac{11709}{193561}$$

$$d_1 = \frac{225645}{1548488}$$

$$d_2 = \frac{-124167}{774244}$$

$$d_{x} = \frac{-2613}{387122}$$

$$d_5 = \frac{13131}{193561}$$

$$d_s = \frac{-28842}{193561}$$

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By further substituting to (46) to (48) we get n_1=\frac{2}{3} n_2=\frac{2}{3} n_3=\frac{4}{3} So we can calculate r_1 and r_2 from (50) and (51), the results are r_1=1 r_2=1 and r_3=1 and r_4=1 and r_5=1 and r_5
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which are exactly the same as our assumption. For a more practical example, the results' accuracy relies heavily on the precision of the software. It needs to be studied that what precision is needed for our test purpose.

## Discussion and conclusions

- In the report, we suppose that two frequencies are used in the measurements. It is noticed that one of them can be zero, that means we can use a DC test and an AC test to identify all the parameters. But in this case, the formulas are more complicated as less information obtained. In fact, a second order, two variables non-linear equation system has to be solved, maybe numerically. Further study is carrying out along this direction hoping find a way to find a relatively simple symbolic solution.
- The calculation can be further reduced as we use two frequencies with one doubles the other, which is the case in the current test system.
- . It is possible to locate leakage fault by using the series resistance.
- The line termination parameters, which are represented by a combined impedance Z in our discussion, can be further identified
- It can be concluded that all the parameters in the enhanced line model can be uniquely identified with two frequencies measurements. For the DC and AC case, the line parameter and the combined line termination can be identified, but the individual line termination parameters remain unsolved

#### Appendix 2

For a two port network as shown in Figure 8 the Z-parameters can be calculated as follows,

$$Z_{11} = r_1 + \frac{1}{g_1 + j\omega c_1} \left( Z + \frac{1}{g_2 + j\omega c_2} \right)$$

$$Z_{11} = r_1 + \frac{1}{g_1 + j\omega c_1} + Z + \frac{1}{g_2 + j\omega c_2}$$

$$= r_1 + \frac{(g_2 + j\omega c_1)Z + 1}{g_1 + g_2 + j\omega c_1 + j\omega c_2 + Z(g_1 + j\omega c_1)(g_2 + j\omega c_2)}$$

$$= r_1 + \frac{(g_2 + j\omega c_2)Z + 1}{\Delta}$$

$$Z_{12} = \frac{\frac{1}{g_1 + j\omega c_1} \frac{1}{g_2 + j\omega c_2}}{\frac{1}{g_1 + j\omega c_1} + Z + \frac{1}{g_2 + j\omega c_2}}$$

$$= \frac{1}{(g_1 + j\omega c)(g_2 + j\omega c_2) \left(\frac{1}{g_1 + j\omega c_1} + Z + \frac{1}{g_2 + j\omega c_2}\right)}$$

$$= \frac{1}{g_1 + g_2 + j\omega c_1 + j\omega c_2 + Z(g_1 + j\omega c_1)(g_2 + j\omega c_2)}$$

$$= \frac{1}{a_1 + g_2 + j\omega c_1 + j\omega c_2 + Z(g_1 + j\omega c_1)(g_2 + j\omega c_2)}$$

$$= \frac{1}{\Delta}$$

$$= \frac{1}{\Delta}$$

$$= \frac{1}{(Z \div \frac{1}{\omega c_1})}$$
(7)

$$Z_{22} = r_2 + \frac{\frac{1}{g_2 + j\omega c_2} \left( Z + \frac{1}{g_1 + j\omega c_1} \right)}{\frac{1}{g_1 + j\omega c_1} + Z + \frac{1}{g_2 + j\omega c_2}}$$

$$= r_2 + \frac{(g_1 + j\omega c_1)Z + 1}{\frac{1}{g_1 + g_2 + j\omega c_1 + j\omega c_2 + Z(g_1 + j\omega c_1)(g_2 + j\omega c_2)}}$$

$$= r_2 + \frac{(g_1 + j\omega c_1)Z + 1}{\frac{1}{g_2 + g\omega c_1 + g\omega c_2 + Z(g_1 + j\omega c_1)(g_2 + j\omega c_2)}}$$
(9)

From (8) we can get

$$Z(g_1 + j\omega c_1)(g_2 + j\omega c_2) = \frac{1}{Z_{12}} - g_1 - g_2 - j\omega c_1 - j\omega c_2$$
 (10)

Rewritten (7) as:

$$Z_{11} = r_1 + [(g_2 + j\omega c_2)Z + 1]Z_{12}$$

multiply 
$$(g_1+i\infty_1)$$
, if  $(g_1+i\infty_1) \neq 0$ , we get

$$\begin{aligned} &(g_1 + j\omega c_1)Z_{11} = r_1(g_1 + j\omega c_1) + (g_1 + j\omega c_1)[(g_2 + j\omega c_2)Z + 1]Z_{12} \\ &= r_1(g_1 + j\omega c_1) + [(g_1 + j\omega c_1)(g_2 + j\omega c_2)Z]Z_{12} + (g_1 + j\omega c_1)Z_{12} \end{aligned} \tag{11}$$

substitute (10) to (11) to eliminate Z,

(13)

$$\begin{split} (g_1 + j\omega c_1)Z_{11} &= r_1(g_1 + j\omega c_1) + (\frac{1}{Z_{12}} - g_1 - g_2 - j\omega c_1 - j\omega c_2)Z_{12} + (g_1 + j\omega c_1)Z_{12} \\ &= r_1(g_1 + j\omega c_1) + 1 - (g_1 + j\omega c_1)Z_{12} - (g_2 + j\omega c_2)Z_{12} + (g_1 + j\omega c_1)Z_{12} \\ &= r_1(g_1 + j\omega c_1) + 1 - (g_2 + j\omega c_2)Z_{12}, \end{split} \tag{12}$$

Similarly we can get an equation about Z22 as

$$(g_2 + j\omega c_2)Z_{22} = r_2(g_2 + j\omega c_2) \div 1 - (g_1 + j\omega c_1)Z_{12}$$

We write the Z-parameters in their real and imaginary part as

 $Z_{11} = Z_{11a} + jZ_{11b}$ 

$$Z_{12} = Z_{12a} + jZ_{12b} \tag{14}$$

 $Z_{n_2} = Z_{n_2} + jZ_{n_3}$ 

Substitute (14) to (12) we get

$$\frac{(g_1 + j\omega c_1)(Z_{11\mu} + jZ_{11\mu})}{(g_1 + j\omega c_1)(Z_{12\mu} + jZ_{12\mu})} = r_1(g_1 + j\omega c_1) + 1 - (g_2 + j\omega c_2)(Z_{12\mu} + jZ_{12\mu})$$

$$g_1Z_{1|\omega} - \omega c_1Z_{1|\omega} + j(g_1Z_{1|\omega} + Z_{1|\omega}\omega c_1) = r_1g_1 + 1 - g_2Z_{12\omega} + \omega c_2Z_{12\omega} + j(r_1\omega c_1 - \omega c_2Z_{12\omega} - g_2Z_{12\omega})$$

By separate real and imaginary part, we get two equations.

$$g_1 Z_{11a} - \omega c_1 Z_{11b} - r_1 g_1 - 1 + g_2 Z_{12a} - \omega c_2 Z_{12b} = 0$$
 (16)

$$g_1Z_{11b} + Z_{11a}\omega c_1 - r_1\omega c_1 + \omega c_2Z_{12b} + g_2Z_{12b} = 0$$
Be substituting (14) to (13) we can get another two equations in a similar way,

$$g_1 Z_{22\mu} - \omega c_2 Z_{12b} - r_2 g_1 - 1 \div g_1 Z_{12\mu} - \omega c_1 Z_{12b} = 0$$
 (18)

$$g_1 Z_{22b} + Z_{22a} \omega c_2 - r_2 \omega c_2 + \omega c_1 Z_{12a} + g_1 Z_{12b} = 0$$
(19)

When the measurements are taken at two frequencies, we can get another set of equation at frequency  $\omega_2$ , if we denote the measurements at this frequency by adding a superscript 2 to the corresponding quantities, the equations can be written as follows

$$g_1 Z_{11a}^2 - \omega_2 c_1 Z_{11b}^2 - r_1 g_1 - 1 + g_2 Z_{12a}^2 - \omega_2 c_2 Z_{12b}^2 = 0$$
(20)

$$g_1 Z_{11b}^2 + Z_{11a}^2 \omega_2^2 c_1 - r_1 \omega_2 c_1 + \omega_2 c_2 Z_{12a}^2 + g_2 Z_{12b}^2 = 0$$
(21)

$$g_2 Z^2_{22a} - \omega_2 c_2 Z^2_{22b} - r_2 g_2 - 1 + g_1 Z^2_{12a} - \omega_2 c_1 Z^2_{12b} = 0$$
(22)

$$g_2 Z^2_{22b} + Z^2_{22a} \omega_2 c_z - r_2 \omega_2 c_z + \omega_2 c_1 Z^2_{12a} + g_1 Z^2_{12b} = 0$$
 (23)

The problem is to solve equations (16) to (23) for model parameters  $r_k$   $g_k$  and  $c_k$ , k=1,2. To eliminate  $r_1$  and  $r_2$ , first let (16) - (20), we get,

$$g_1(Z_{11a} - Z_{11a}^2) - c_1(\omega Z_{11b} - \omega_2 Z_{11b}^2) + g_2(Z_{12a} - Z_{12a}^2) - c_2(\omega Z_{12b} - \omega_2 Z_{12b}^2) = 0$$
(24)

then  $\omega_1 \times (17) = \omega_1 \times (21)$  which gives

$$g_{1}\left(\omega_{2}Z_{11b}-\omega Z_{11b}^{2}\right)-\omega\omega_{2}c_{1}\left(Z_{11a}-Z_{11a}^{2}\right)+g_{2}\left(\omega_{2}Z_{12b}-\omega Z_{12b}^{2}\right)-\omega\omega_{2}c_{2}\left(Z_{12a}-Z_{12a}^{2}\right)=0\tag{25}$$

similarly, (12) - (16) yields.

$$g_1(Z_{12a} - Z_{12a}^1) - c_1(\omega Z_{12b} - \omega_1 Z_{12b}^1) + g_1(Z_{12a} - Z_{12a}^1) - c_1(\omega Z_{12b} - \omega_2 Z_{12b}^2) = 0$$
 (26)  
Let.

$$a_{t} = Z_{t|a} - Z_{t|a}^{2} \tag{27}$$

$$a_2' = Z_{12a} - Z_{12a}^2 \tag{28}$$

$$a_3 = Z_{22} - Z_{22}^2 \tag{29}$$

$$b_1 = \omega Z_{11b} - \omega_2 Z_{11b}^2 \tag{30}$$

$$b_2 = \omega_1 Z_{11b} - \omega Z_{11b}^2$$
 (31)

$$b_3 = \omega Z_{125} - \omega_2 Z_{125}^2 \tag{32}$$

$$b_4 = \omega_2 Z_{12b} - \omega Z_{12b}^2$$
 (33)

$$b_s = \omega Z_{22b} - \omega_z Z_{22b}^2 \tag{34}$$

$$b_6 = \omega_2 Z_{22b} - \omega Z_{22b}^2 \tag{35}$$

So (24) to (26) can be rewritten as

$$a_1g_1 - b_1c_1 + a_2g_2 - b_3c_2 = 0 (36)$$

$$b_2 g_1 \div a_1 \omega \omega_2 c_1 + b_4 g_2 + a_2 \omega \omega_2 c_2 = 0$$

$$a_1 g_1 - b_2 c_2 + a_2 g_1 - b_2 c_1 = 0$$
(37)

 $a_1g_2 - a_3c_2 + a_2g_1 - a_3c_1 = 0$ Solve (36) to (38) for  $g_1$ ,  $c_1$ , and  $c_2$  we get,

Solve (30) to (38) for g1, c1, and c2 we get,

$$g_{1} = -\frac{a_{1}a_{2}b_{2}\omega\omega_{2} + b_{2}b_{3} - (b_{3})^{2}b_{4} + a_{1}a_{2}b_{1}\omega\omega_{2} - a_{1}a_{2}b_{2}\omega\omega_{2} - (a_{2})^{2}b_{3}\omega\omega_{2}}{\Delta_{1}}g_{2}$$
(39)

$$\frac{a_{i}b_{i}b_{i} + a_{i}a_{i}a_{i}\omega\omega \cdot - a_{i}b_{i}b_{i} - (a_{i})^{3}\omega\omega \cdot - a_{i}b_{i}b_{i} + a_{i}b_{i}b_{i}}{\Delta_{1}} g_{2}$$
(46)

$$c_{2} = \frac{-a_{2}b_{1}b_{2} + a_{3}b_{1}b_{2} - a_{1}(a_{2})^{2}\omega\omega_{2} - a_{2}b_{2}b_{3} + (a_{1})^{2}a_{3}\omega\omega_{2} + a_{3}b_{2}b_{4}}{\Delta_{1}}g_{2}$$
(41)

where

$$\Delta_{1} = b_{1}b_{2}b_{3} + (a_{1})^{2}b_{3}\omega\omega_{2} - b_{2}(b_{3})^{2} + (a_{2})^{2}b_{1}\omega\omega_{2} - 2a_{1}a_{2}b_{2}\omega\omega_{2}$$

$$(42)$$

If we denote the coefficient of (39)-(41) by  $n_j$  j=1, 2,3, we get,

$$g_1 = n_1 g_2$$
 (43)  
 $c_1 = n_2 g_3$  (44)

$$c_1 = n_2 g_2 \tag{44}$$

$$c_2 = n_1 g_2 \tag{45}$$

vhere

$$n_{i} = -\frac{a_{i}a_{2}b_{i}\omega\omega_{z} + b_{i}b_{z}b_{z} - (b_{z})^{2}b_{z} + a_{z}a_{z}b_{i}\omega\omega_{z} - a_{z}a_{z}b_{i}\omega\omega_{z} - (a_{z})^{2}b_{z}\omega\omega_{z}}{\Delta_{i}}$$
(46)

$$n_{2} = -\frac{a_{1}b_{2}b_{3} + a_{1}a_{2}a_{2}\omega\omega_{2} - a_{2}b_{2}b_{3} - (a_{2})^{3}\omega\omega_{2} - a_{2}b_{3}b_{4} + a_{2}b_{2}b_{3}}{\Delta}$$
(47)

$$n_{3} = \frac{-a_{2}b_{1}b_{4} + a_{2}b_{1}\dot{b}_{2} - a_{1}(a_{2})^{2}\omega\omega_{2} - a_{2}b_{2}b_{3} + (a_{1})^{2}a_{2}\omega\omega_{2} + a_{2}b_{2}b_{4}}{\Delta_{1}}$$

$$(48)$$

Substitute  $g_1, c_1, c_2$  to (17)

$$n_1 g_2 Z_{11b} + Z_{11a} \omega n_2 g_2 - r_1 \omega n_2 g_2 + \omega n_3 g_2 Z_{12a} + g_2 Z_{12b} = 0$$

$$\tag{49}$$

if  $g_2 \neq 0$ , we can solve (49) for  $r_1$  as follows

$$\tau_{1} = \frac{n_{1}Z_{11b} + Z_{11a}\omega n_{2} + \omega n_{2}Z_{12a} + Z_{12b}}{\omega n_{2}}$$
(50)

Similarly we can get r<sub>2</sub> from (19)

$$r_{z} = \frac{n_{z}Z_{11b} + Z_{22a}\omega n_{z} + \omega n_{z}Z_{12a} + Z_{22b}}{\omega n_{z}}$$
(51)

Substitute  $g_1, c_1, c_2$  and  $r_1$  to (16), we can determine  $g_2$ .

$$g_{z} = -\frac{\omega n_{z}}{(n_{z})^{2} Z_{1b} + n_{z} n_{z} Z_{12a} \omega + n_{z} Z_{12b} - n_{z} Z_{12a} \omega + n_{z} n_{z} Z_{12b} (\omega)^{2} + (n_{z})^{2} Z_{1b} (\omega)^{3}}$$
(52)

After  $g_2$  is determined,  $g_1, c_1, c_2$  can be calculated from (43) to (45). So far, the only parameter left undetermined is Z, which can be calculated at frequency  $\omega$  from (10) as

$$Z = \frac{\frac{1}{Z_{12}} - g_1 - g_2 - j\omega c_1 - j\omega c_2}{(g_1 + j\omega c_1)(g_2 + j\omega c_2)}$$
(53)

#### Appendix 3

## Further discussions on Identification Results

In Appendix 2 we got a set of symbolic solutions to all the parameters in the enhanced model. The results are repeated here,

$$r_{1} = \frac{n_{1}Z_{11s} + Z_{11s}\omega n_{2} + \omega n_{2}Z_{12s} + Z_{12s}}{\omega n_{2}}$$
(1)

$$r_{2} = \frac{n_{1}Z_{11b} + Z_{22a}\omega n_{1} + \omega n_{2}Z_{12a} + Z_{22b}}{\omega n_{2}}$$
(2)

$$g_{2} = -\frac{\omega n_{2}}{(n_{1})^{2} Z_{1:b} + n_{1} n_{2} Z_{1:a} \omega + n_{1} Z_{1:a} \omega + n_{2} Z_{1:a} \omega + n_{2} Z_{1:a} (\omega)^{2} + (n_{2})^{2} Z_{1:b} (\omega)^{3}}$$
(3)

$$g_1 = n_1 g_2$$

$$c_1 = n_2 g_2 \tag{4}$$

$$c_2 = n_3 g_2 \tag{5}$$

$$Z = \frac{\frac{1}{Z_{12}} - g_1 - g_2 - j\omega c_1 - j\omega c_2}{(g_1 + j\omega c_1)(g_2 + j\omega c_2)}$$
(6)

where  $\omega$  is test frequency,  $Z_{ija}$  and  $Z_{ijb}$  i=1,2, j=1,2 are the real and imaginary parts of the Z-parameters respectively, and  $n_b$  k=1,2,3 can be calculated as follows,

$$n_{1} = -\frac{a_{1}a_{2}b_{2}\omega\omega_{2} + b_{1}b_{2}b_{2} - (b_{2})^{2}b_{1} + a_{2}a_{2}b_{1}\omega\omega_{2} - a_{1}a_{2}b_{3}\omega\omega_{2} - (a_{2})^{2}b_{3}\omega\omega_{2}}{\Delta_{2}}$$
(7)

$$n_{z} = -\frac{a_{z}b_{z}b_{z} + a_{1}a_{z}a_{z}\omega\omega_{z} - a_{z}b_{z}b_{z} - (a_{z})^{3}\omega\omega_{z} - a_{z}b_{z}b_{z} + a_{z}b_{z}b_{z}}{\Delta_{1}}$$
(3)

$$n_{2} = \frac{-a_{2}b_{1}b_{4} + a_{2}b_{2}b_{2} - a_{1}(a_{2})^{2}\omega\omega_{2} - a_{2}b_{2}b_{2} + (a_{1})^{2}a_{3}\omega\omega_{2} + a_{1}b_{2}b_{4}}{\Delta_{1}}$$
(9)

where

$$\Delta_{1} = b_{1}b_{2}b_{3} + (a_{1})^{2}b_{2}\omega\omega_{2} - b_{2}(b_{3})^{2} + (a_{2})^{2}b_{1}\omega\omega_{2} - 2a_{1}a_{2}b_{3}\omega\omega_{2}$$
(10)

and  $a_k$ , k=1,2,3,  $b_j$ , j=1...6 can be calculated directly from the knowns (See [1] for thei definations)

One problem with this set of formula is that  $\Delta_1$  can be zero for some particular measurement values. In this case, an alternative has to be found to calculate the parameters. Taking into

consideration the condition that  $\Delta_t$  is zero, another set of formula can be obtained as shown in the follows.

$$r_{i} = -\frac{-Z_{11a}\omega a_{2}b_{5} + Z_{11a}\omega a_{5}b_{5} - Z_{12b}b_{5} + Z_{12b}(b_{5})^{2} - Z_{12a}\omega a_{3}b_{1} + Z_{12a}\omega a_{2}b_{3}}{\omega(a_{2}b_{3} - a_{3}b_{3})}$$
(11)

$$r_{2} = \frac{Z_{22a}\omega a_{1}b_{3} - Z_{22a}\omega a_{2}b_{1} - Z_{12b}b_{1}b_{3} + Z_{12b}(b_{3})^{2} - Z_{12a}\omega a_{1}b_{5} + Z_{12a}\omega a_{2}b_{3}}{\omega(a_{1}b_{3} - a_{2}b_{1})}$$
(11)

$$g_1 = \frac{s_2 - m_2}{m_1 s_2 - m_2 s_1} \tag{13}$$

$$c_2 = \frac{m_1 - s_1}{m_1 s_1 - m_2 s_1} \tag{14}$$

$$c_1 = q_1 c_2 + q_2 g_2 \tag{15}$$

$$c_1 = p_1 c_2 + p_2 g_2 \tag{16}$$

where

$$m_1 = Z_{11a}p_2 - \omega Z_{11b}q_2 - r_1p_2 + Z_{12a}$$
 (17)

$$m_2 = Z_{11a}p_1 - \omega Z_{11b}q_1 - r_1p_1 + \omega Z_{12b}$$
 (18)

$$s_1 = Z_{22a} - r_2 + Z_{12a} p_2 - \omega Z_{12b} q_2 \tag{19}$$

$$s_{2} = -\omega Z_{22b} + Z_{12a} p_{1} - \omega Z_{12b} q_{1}$$
 (20)

and

$$p_{1} = \frac{(b_{3})^{2} - b_{1}b_{3}}{a.b. - a.b.} \tag{21}$$

$$p_2 = \frac{a_1b_1 - a_2b_1}{a_1b_1 - a_2b_1} \tag{22}$$

$$q_1 = \frac{a_2b_3 - a_1b_5}{a_1b_2 - a_2b_3} \tag{23}$$

$$q_2 = \frac{a_1 a_3 - (a_2)^2}{a_1 b_1 - a_2 b_2} \tag{24}$$

#### Appendix 4

### Line termination

The line is usually terminated by a resistance R in series with a capacitor C, which is paralleled by the loop resistance and capacitors. To determine the termination is to identify all these parameters. In Appendix 1 and 2 we have got the equivalent impedance Z or admittance of the termination Y at two frequencies when we identify the model parameters. We now considering using admittance representation. From Figure 9 we have

$$Y = g + j\omega c_1 + \frac{j\omega c_2}{1 + j\omega Rc_2}$$
 (1)

Let

$$Y = a + ib \tag{2}$$

where a and b are the real and imaginary part of Y respectively. So

$$a = g + \frac{\omega^2 R c_z^2}{1 + \omega^2 R^2 c_z^2}$$
 (3)

$$b = \omega c_1 + \frac{\omega c_2}{1 + \omega^2 R^2 c_2^2} \tag{4}$$

Let

$$Rc_{\gamma} = x \tag{5}$$

and measure the Y at two frequencies  $\omega_1$  and  $\omega_1$ , we have

$$a_1 - a_2 = \frac{\omega_1^2 x c_2}{1 + \omega_1^2 x^2} - \frac{\omega_{21}^2 x c_2}{1 + \omega_1^2 x^2}$$
 (6)

and

$$\frac{b_1}{\omega} - \frac{b_2}{\omega} = \frac{c_2}{1 + \omega_1^2 x^2} - \frac{c_2}{1 + \omega_2^2 x^2}$$
(7)

(6)/(7) we have

$$\frac{a_1 - a_2}{\frac{b_1}{\omega_1} - \frac{b_2}{\omega_2}} = \frac{\frac{\omega_1^2 x}{1 + \omega_1^2 x^2} - \frac{\omega_2^2 x}{1 + \omega_2^2 x^2}}{\frac{1}{1 + \omega_1^2 x^2} - \frac{1}{1 + \omega_2^2 x^2}}$$

$$= x \frac{\omega_1^2 (1 + \omega_1^2 x^2) - \omega_2^2 (1 + \omega_1^2 x^2)}{(1 + \omega_2^2 x^2) - (1 + \omega_1^2 x^2)}$$

$$= x \frac{\omega_1^2 - \omega_2^2}{\omega_2^2 x^2 - \omega_1^2 x^2}$$

$$= -\frac{1}{2}$$
(8)

i.e

$$x = -\frac{\frac{b_1}{\omega_1} - \frac{b_2}{\omega_2}}{a_1 - a_2} = \frac{1}{\omega_1 \omega_2} \frac{\omega_2 b_1 - \omega_1 b_2}{a_2 - a_1}$$
 (9)

After we get x, c2 can be calculated from (6), which gives

$$c_2 = \frac{(a_1 - a_2)(1 + \omega_1^2 x^2)(1 + \omega_2^2 x^2)}{x(\omega_1^2 - \omega_2^2)}$$
(10)

and R from (5)

$$R = \frac{x}{c_s} \tag{11}$$

So g and c1 can be determined from (3) and (4) respectively

$$g = a_1 - \frac{\omega_1^2 x c_2^2}{1 + \omega_1^2 x^2}$$
(12)

and

$$c_1 = \frac{b_1}{\omega_1} - \frac{c_2}{1 + \omega_1^2 x^2} \tag{13}$$

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#### CLAIMS

- A method of testing a telecommunications system, the method comprising;
- applying a first AC test signal having a first signal frequency to the system and measuring the response of the system to the first test signal;
- 2) applying a second AC test signal having a second signal frequency different to the first signal frequency to the system and measuring the response of the system to the second test signal; and
- 3) calculating one or more parameters of the system from the responses measured in steps 1) and 2).
- A method according to claim 1 wherein the first and second test signals are applied at different times.
- 3. A method according to claim one or two wherein one or both of the test signals has a substantially sinusoidal waveform.
- 4. A method according to any of the preceding claims wherein less than five cycles of each signal is applied to the system.
- 5. A method according to any of the preceding claims wherein the test signals are each applied to the system through a known impedance.
- 6. A method according to any of the preceding claims further comprising applying;
- 4) applying one or more additional test signals to the system and measuring the response of the system to the or each test signal; and

wherein step 3) comprises calculating one or more parameters of the system from the responses measured in steps 1),2) and 4).

- 7. A method according to any of the preceding claims wherein the system comprises first and second transmission lines, and wherein each step of applying a test signal and
- 35 measuring the response of the system comprises

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- applying the test signal to the first line and monitoring the response of the first line and the second line to the test signal; and
- applying the test signal to the second line and monitoring the response of the second line and the first line to the second test signal.
  - A method of testing a telecommunications system comprising first and second transmission lines, the method comprising
- 1) applying a first test signal to the first line and measuring the response of the first line and the second line to the first test signal;
- applying a second test signal to the second line and measuring the response of the second line and the first line to the second test signal; and
- calculating one or more parameters of the telecommunications system from the responses measured in steps 1) and 2).
- 9. A method according to any claim 8 wherein the first and second signals each comprise AC signals.
- 10. A method according to claim 9 wherein the signal frequencies of the first and second test signals are substantially identical.
- 11. A method according to claim 10 wherein the first and 25 second test signals have a known phase relationship.
  - 12. Apparatus for testing a telecommunications system, the apparatus comprising;
  - means for applying a first AC test signal having a first signal frequency to the system;
- means for measuring the response of the system to 30 the first test signal;
  - means for applying a second AC test signal having a second signal frequency different to the first signal frequency to the system;
- means for measuring the response of the system to 35 the second test signal; and

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- 5) means for calculating one or more parameters of the system from the responses measured in steps 1) and 2). 13. Apparatus for testing a telecommunications system comprising first and second transmission lines, the apparatus comprising
- 1) means for applying a first test signal to the first line  $% \left( \frac{1}{2}\right) =\frac{1}{2}\left( \frac{1}{$
- means for measuring the response of the first line and the second line to the first test signal;
- means for applying a second test signal to the second line
  - 4) means for measuring the response of the second line and the first line to the second test signal; and
  - 5) means for calculating one or more parameters of the telecommunications system from the responses measured in steps 1) and 2).

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(21) International Application Number: PCT/US (22) International Filing Date: 26 May 1999 ( (30) Priority Data: 98304171.6 27 May 1998 (27.05.98)  (71) Applicant I for all designated States except US): POR TEMS CORPORATION [US/US]; 575 Underhivard, Syosset, NY 11791 (US).  (72) Inventors; and (75) Inventors/Applicants (for US only): DE TULLIG [GB/GB]; 6 Beech Cliffe. Warwick CV34 5F GREENING, Mark (DB/GB); 140 FEMEL, Pohr [GB/GB]; 160 FEMEL, John [GB/GB]; 160 FEMEL, John [GB/GB]; 160 FEMEL, John [GB/GB]; 161 FEMEL HOLD, TOK 19T (GB).  (74) Agent: ZUSCHLAG, Steven, T.; Hoffmann & Bar 6900 Jericho Turmpike, Syosset, NY 11791 (US).	TA SY II Bou D, Rob IY (Glue, Ken II Dam D, Kelv DB (Gl	BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES, FI, GB, SG, GE, GH, GM, RH, HU, DI, LI, NI, SI, PY, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, GS, SI, SK, SI, TI, TM, TR, TT, UA, UG, US, UZ, VN, YU, ZA, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SL, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, SS, FI, FR, GB, GR, IE, IT, LU, MC, NI, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).  Published  Without international search report and to be republished upon receipt of that report.			
(54) Title: APPARATUS AND METHOD FOR TESTING A TELECOMMUNICATIONS SYSTEM					
		nethod comprising: 1) applying a first AC test signal having a first signal em to the first test signal; 2) applying a second AC test signal having a			

A method of testing a telecommunications system (/), the method comprising: 1) applying a next AC test signal having an ris signal frequency to the system and measuring the response of the system to the first test signal; 2) applying a second AC test signal having a second signal frequency different to the first signal frequency to the system and measuring the response of the system to the second test signal; and 3) calculating one or more parameters of the system from the responses measuring the response of the system to the second test signal; and 3) calculating one or more parameters of the system from the responses measuring in steps 1) and 6).

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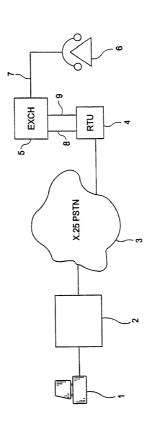
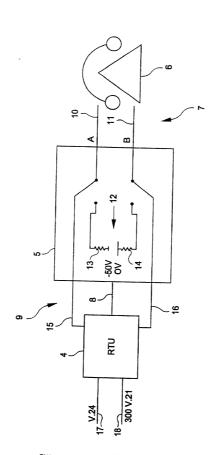


FIG-1

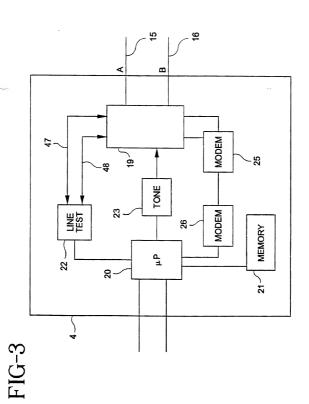




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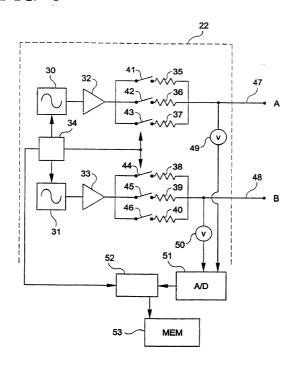


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## FIG-4



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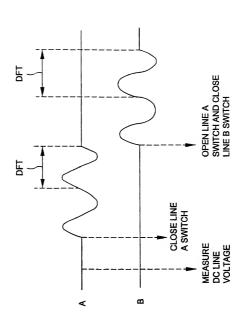
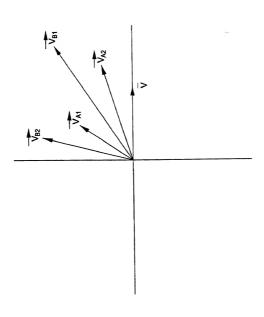


FIG-



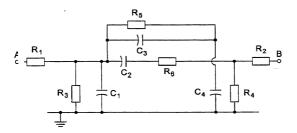
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FIG-6

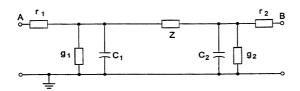
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FIG-9

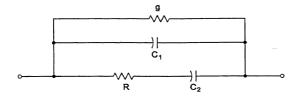
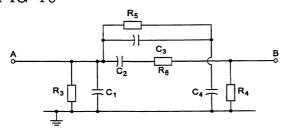


FIG-10



Page 1 of 2

## VERIFIED STATEMENT (DECLARATION) CLAIMING SMALL ENTITY

STATUS (37 (	CFR 1.9(f)	AND 1.27 (c)) - SMAL	LL BUSINESS CONCERN	587-68 EPO/PCT/US	
Serial No.		Filing Date	Patent No.	Issue Date	
PCT/US99/1161	7	May 26, 1999	,	loodo Balo	
Applicant/ Robert De Tullio, et al. Patentee:					
Invention: APPAR	ATUS AND N	METHOD FOR TESTING	A TELECOMMUNICATIONS	SYSTEM	
I hereby declare that	t I am:				
		business concern identifie	d helow:		
an official o	of the small t	ousiness concern empowe	ered to act on behalf of the conc	em identified below:	
NAME OF CONCER					
ADDRESS OF CON	CERN: 575 I	Underhill Boulevard, Syoss	et. New York 11791		
44					
I hereby declare that	the above-io	dentified small business or	oncem qualifies as a small busi ourposes of paying reduced fee	ness concern as defined in	
(LD) OF THE 35, UTILE	a States Cod	de, in that the number of a	employees of the concern inclu	iding those of its offiliates	
poes not exceed 500	persons. F	or purposes of this statem	ent (1) the number of employed	as of the husiness sensem	
temporary basis dun	ng each of the	he pay periods of the fisc:	ern of the persons employed of al year, and (2) concerns are af	filiator of ooob atherbeen	
either, directly or inc controls or has the po	airectly, one	concern controls or has t	the power to control the other,	or a third party or parties	
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concern identified ab	ove with reg	der contract or law have ard to the above identified	been conveyed to and remain invention described in:	n with the small business	
☐ the spec	ification filed	d herewith with title as liste	ed above.		
the appli	ication identi	ified above.			
☐ the pate	nt identified	above.			
If the rights held by	the above-i	identified small business	concern are not exclusive, ea	ch individual, concern or	
organization naving r	ngnts to the	invention is listed on the	next page and no rights to the an independent inventor under	invention are held by any	
CONCERN WHICH WOULD	not qualify a	as a small business conce	em under 37 CFR 1.9(d) or a no	37 CFR 1.9(c) or by any	
37 CFR 1.9(e).			(-,	The signification and of	

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Each person obligation und	, concern d der contract	or organiza or law to a	tion to which I ssign, grant, co	have assigned, granted, co nvey, or license any rights in	nveyed, or l the invention	icensed or am under a on is listed below:
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hereby decl	are that all	statement	s made herein	of my own knowledge are t	rue and that	all statements made of
willful false st	atements a	nd the like	so made are ou	further that these statement	s were made	with the knowledge the
Title to Ut ti	ne United :	States Cod	ie, and that su	ich willful false statements nt to which this verified state	may jaona	rdiza the validity of th
	ny patoni io	oung there	on, or any pare	nicio which this verified state	ement is direc	cted.
NAME OF PER	RSON SIGN	IING:	William V. Ca	arney		
TITLE OF PER	SON SIGN	ING				
OTHER THAN	OWNER:		Chairman of t	he Board and Chief Executiv	e Officer	
ADDRESS OF	PERSON S	SIGNING:	575 Underhill	Boulevard		
			Syosset, New	York 11791		
	-1	1.0	1.0			
SIGNATURE:	NU	lliam	e V. Car	Mely DATE:	12-21	-00
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the specification of which

# Declaration and Power of Attorney For Patent Application English Language Declaration

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name,

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled

APPARATUS AND METHOD FOR TESTING A TELECOMMUNICATIONS SYSTEM

(check one)			
a is attached here			
a. was filed on Ma		as United States Application No	or PCT International
Application Num	ber PCT/US99/11617		
and was amend	ed on		
New York		(if applicable)	
	have reviewed and ur	nderstand the contents of the above i	dentified specification.
including the claims	, as amended by any :	amendment referred to above.	
known to me to be Section 1,56. I hereby claim fore Section 365(b) of a	<ul> <li>material to patentab</li> <li>ign priority benefits to</li> <li>iny foreign application</li> </ul>	United States Patent and Trademan filly as defined in Title 37, Code of under Title 35, United States Code, (is) for patent or inventor's certificate of designated at least one country of	Federal Regulations, Section 119(a)-(d) or to or Section 365(a) of
States, listed below	and have also identificate or PCT into priority is claimed.	fied below, by checking the box, any emational application having a filing o	foreign application for
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J. Catanzaro, Reg. No. 25,937; Lauren T. Emr, Reg. No. 46,139; James F. Harrington, Reg. No. 46,139; Junia K. Holmes, Reg. No. 36,074; Junia K. Holmes, Reg. No. 42,666; Kevin E. McDermott, Reg. No. 55,946; Robert C. Morriss, Reg. No. 42,910; R. Glean Schroeder	Buron, Reg. No. 45,150; Barry Jacobsen, Reg. No. 43,689; Kellyanne Merkel, Reg. No. 43,680; John S. Sopke, Reg. No. 41,321; Gloria K. Szukiel, Reg. No. 45,149; E. H. G. H.
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Great Britain Poel Office Address same as above	
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Full name of fourth Inventor, if any John Kelvier Eidler	
Fourth invertor's signature	19/01/01
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Great Britain	
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